



## Research Article

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# Removal of Heavy Metal Cations (Copper, Lead, Zinc) from Water Runoff by Calcium Silicate Hydrate: Effect of the Co-Ion and Competition of Ions in Ternary Mixtures

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## Abstract

The sorption behavior of calcium silicate hydrate (CSH) with respect to lead, copper and zinc was studied to consider its application to remove metal from water runoff. A series of kinetics of removal and isotherms were undertaken with single metal and mixture solutions. The sorption occurred by ion exchange with calcium. Sorption kinetics were modelled using pseudo-second order model. The weight capacities of CSH were lead > copper >> zinc when studied separately. The co-ion associated to the metal ion is of importance on the removal capacities. Langmuir-Freundlich isotherm model matched experimental data in the case of single metal solutions. A competition was evidenced in mixture; zinc was the most impacted.

## Keywords

Surface water runoff treatment, Heavy metal removal, Calcium silicate hydrate, Cation exchange, Sorption kinetics and isotherms

## Highlights

- Performances of calcium silicate hydrate (CSH) to capture metal ions are evaluated
- Retention capacities in  $\text{mg}_{\text{metal}} \cdot \text{g}_{\text{CSH}}^{-1}$  follows the order  $\text{Pb(II)} > \text{Cu(II)} >> \text{Zn(II)}$
- Removal kinetics and isotherms are properly modeled by pseudo-second order model and Langmuir-Freundlich model respectively
- The co-ion associated to the metal is of importance on the removal capacity
- Retention capacities for Cu, Pb and Zn decrease in the case of a ternary metal mixture

## Introduction

Water pollution caused by organic and inorganic compounds is a world issue originated by natural and anthropogenic sources. Experience with metals showed that they can give rise to specific concerns due to their potential to accumulate in parts of the environment and their potential toxic effects on animals, plants and humans [1]. Some of them are even now included in the list of priority pollutants:

- Four heavy metals (cadmium, lead, mercury and nickel) in the list of priority pollutants of the European Union Water Framework Directive 2000/60/Ec [2]

- Thirteen heavy metals (antimony, arsenic, beryllium, cadmium, chromium, copper, lead, mercury, nickel, selenium, silver, thallium and zinc) in the list of priority pollutants of the US Environmental Protection Agency (EPA) [3].

Even if all of heavy metals are present in the Earth crust, their wide presence in waters, soils and atmosphere is mainly due to human activities (industries, car traffic, urbanization,...) and can affect the quality and ecology of receiving waters [4-6]. Storm water runoff has been identified as a main cause of pollutant diffusion in the environment [7-9]. For example, motor vehicle emissions and vehicle tire wears are some of diffuse sources of chemical contaminants in urban environments [10]. During rainfalls, these chemical contaminants are washed out from different surfaces such as roofs and roads

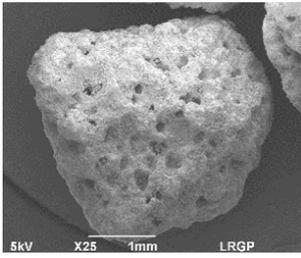
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**Table 1:** CSH elemental analysis.

	Composition (weight %)					
	SiO <sub>2</sub>	Al <sub>2</sub> O <sub>3</sub>	Fe <sub>2</sub> O <sub>3</sub>	MnO	MgO	CaO
	58.67	0.36	0.12	< D.L. <sup>(1)</sup>	0.34	29.64
	Na <sub>2</sub> O	K <sub>2</sub> O	TiO <sub>2</sub>	P <sub>2</sub> O <sub>5</sub>	LOI <sup>(2)</sup>	Total
	< D.L.	< D.L.	< D.L.	< D.L.	12.30	101.41

<sup>(1)</sup> < D.L.: Below the detection limit; <sup>(2)</sup> LOI: Loss of ignition at 1000 °C.

into the stormwater system [7,10]. Heavy metals such as copper (Cu(II)), lead (Pb(II)) and zinc (Zn(II)) are of particular concern in such runoff due to their occurrence, toxicity to aquatic organisms and persistence in the environment [5,11,12].

To remove heavy metal ions from water, several processes exist such as sorption [13-15], phytoextraction [1,16,17], ultrafiltration [18,19] and reverse osmosis [20]. Sorption techniques are often used due to their simplicity as well as the availability of a wide range of sorbents [21]. Materials such as activated carbons, zeolites and calcium silicate hydrates (CSH) have been used to remove heavy metals from water [14,22-26].

According to Zhao, et al. [24], CSH received attention by means of their excellent bioactivity and biocompatibility. Some studies were carried out to explore their applications in drug delivery and sorption of heavy metal ions. Chen, et al. [25] showed that this low-cost material is a promising sorbent for Pb(II), Cu(II), Zn(II) and Cr(III) ion removal from aqueous solutions with sorption capacities between 31 and 94 mg<sub>Metal</sub>·g<sub>CSH</sub><sup>-1</sup>. Ma, et al. [26] studied the capture of Ni(II), Cu(II), Zn(II) and Co(II) ions from aqueous solutions and showed the potential of a CSH, by-product of alumina production. The announced capacities reached values between 240 and 700 mg<sub>Metal</sub>·g<sub>CSH</sub><sup>-1</sup>.

In this paper, the performance of one kind of CSH for the removal of three heavy metals (copper, lead and zinc) was evaluated when present alone but also in mixture in water. Among the objectives, a special focus was addressed to the comprehension of the retention mechanisms, the analysis of competition phenomena, and the influence of the nature the co-ions present in solution. This experimental study, based on kinetics and thermodynamics approaches, is the first step in the conception and development of an innovative *in-situ* treatment solution integrated into the water runoff management system.

## Materials and Methods

### Characterization of the CSH

The studied calcium silicate hydrate (CSH) is a commercial ~3 mm-granular CSH with a Ca/Si ratio equal to 0.77 (Table 1) and used as received. CSH samples were characterized (before and after metal sorption) by Scanning Electron Microscopy (SEM; JEOL JSM-6490LV, Jeol, Japan) coupled to a module of Energy Dispersive X-ray Spectrometry (EDX) (NumeriX DXP-

X10P digital X-ray processor, SamX, France). The preparation of each sample was based on the fixation of an Au-Pd thin layer using an ion sputter (Fine Coat Ion Sputter JFC-1100, Jeol, Japan). Observations of the samples were conducted using 5 kV of accelerating voltage. The EDX analyses were conducted with 20 kV accelerating voltage.

The elemental composition of ground samples (< 80 µm) was analyzed by ICP-OES (inductively coupled plasma - optical emission spectrometry) after alkaline fusion and acidic dissolution by the SARM analytical research facility (CRPG, CNRS, Nancy). Weight percent compositions were expressed as oxidized form (Table 1). The loss on ignition at 1000 °C (corresponding mainly to organic matter, carbonates and water) was also given. A textural analysis by nitrogen adsorption at 77 K (Tristar II, Micromeritics) revealed that the CSH material is not microporous.

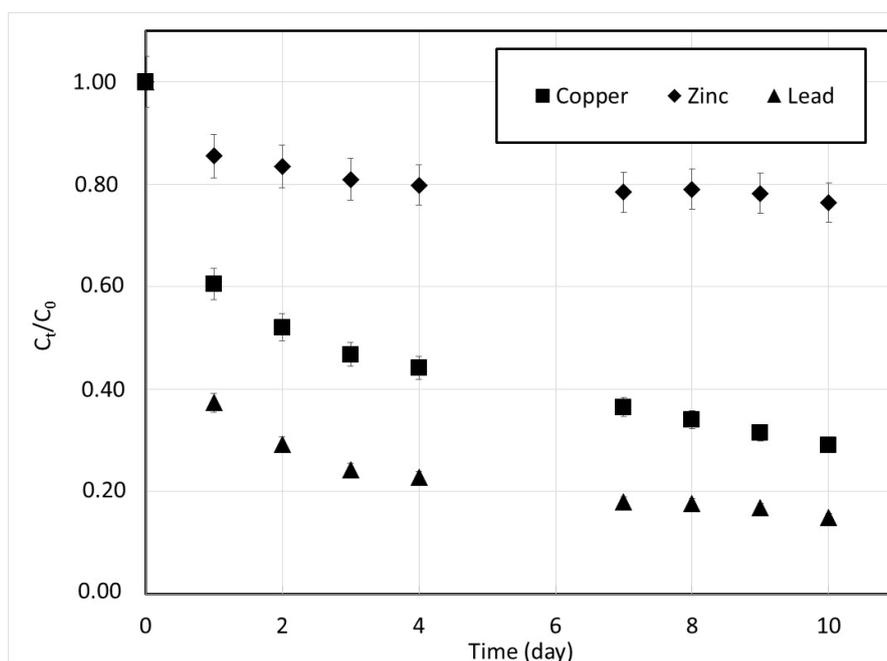
### Reagents

The studied metal ions were Cu(II), Zn(II) and Pb(II). All compounds were analytical-grade reagents with purity higher than 98%. Synthetic solutions of Cu(II), Zn(II) and Pb(II) were prepared using nitrate salts or sulfate salts in ultrapure water. Cu(NO<sub>3</sub>)<sub>2</sub>·3H<sub>2</sub>O, Zn(NO<sub>3</sub>)<sub>2</sub>·6H<sub>2</sub>O were supplied by Acros Organic (USA) and Pb(NO<sub>3</sub>)<sub>2</sub>, CuSO<sub>4</sub>·5H<sub>2</sub>O and ZnSO<sub>4</sub>·7H<sub>2</sub>O were supplied by VWR BDH Prolabo (UK). Nitric acid was used to acidify the samples before analysis by ICP-OES. Nitric acid (67-70%) of ICP-OES quality was purchased from Fisher Scientific (USA).

### Batch sorption studies

In order to simplify the notations, all masses, volumes, concentrations and sorption capacities will always refer to a metal mass in milligram, a solution volume in liter (or mL) and a CSH mass in gram.

**Kinetics experiments:** Solutions containing metal ions at 3000 mg·L<sup>-1</sup> were prepared. Batch sorption kinetics experiments were conducted at 22 °C by contacting 200 mL of solution with a known amount of CSH in 240-mL LDPE bottles. The bottles were shaken in an orbital shaker (STARLAB). Aqueous samples were taken at different time intervals until the equilibrium was reached. Aqueous samples were filtered through a 0.45 µm nylon filter (VWR, UK), diluted if necessary with ultrapure water and then acidified to 2% with HNO<sub>3</sub> for analysis by ICP-OES (ICAP 6300 DUO, Thermo Scientific, USA). Absorption wavelengths used were 224.7 nm for Cu(II), 202.5



**Figure 1:** Long-term kinetics for copper, lead and zinc removal from single metal solutions containing nitrates using CSH (T = 22 °C, C<sub>0</sub> = 3000 mg.L<sup>-1</sup>, V = 200 mL, m<sub>CSH</sub> = 2.5 g).

nm for Zn(II) and 220.3 nm for Pb(II).

**Sorption isotherms:** The sorption isotherms of heavy metals on CSH were carried out using the batch method to evaluate the equilibrium capacities of the material. Isotherms at 22 °C were obtained by contacting 200 mL of heavy metal ion solution (3000 mg.L<sup>-1</sup>) with various masses of CSH ranging from 0.5 g to 40 g in 240-mL LDPE bottles. The bottles were shaken in an orbital shaker (STARLAB) until the equilibrium was attained. Finally, a 10 mL supernatant liquid volume of each sample was filtered, diluted if necessary, acidified and analyzed by ICP-OES as described in the previous paragraph.

The amount of metal retained was calculated by:

$$q_t = \frac{(C_0 - C_t) \cdot V}{m_{\text{CSH}}} \quad (\text{eq.1})$$

where  $q_t$  is the amount of metal retained at time  $t$  (mg.g<sup>-1</sup>),  $C_0$  is the metal initial concentration in solution (mg.L<sup>-1</sup>),  $C_t$  is the metal concentration in solution at time  $t$  (mg.L<sup>-1</sup>),  $V$  is the volume of the solution (L) and  $m_{\text{CSH}}$  is the mass of CSH used (g). This capacity can be calculated when the equilibrium is reached and will be noted  $q_e$ .

Most of experiments were carried out twice to check the reproducibility of the results. CSH-free blanks and metal-free blanks were used as controls. Based on the replicates, the maximum error on the capacities was estimated to  $\pm 10\%$ .

## Results and Discussion

### Single metal solutions from nitrate salts

**Kinetics experiments:** Kinetics measurements were conducted by following the decrease of the metal concentration

in the liquid phase (Figure 1). The measurements were carried on for a long time (ten days) with rather small amounts of CSH (2.5 g). As expected for liquid, the sorption rate for each metal, represented by the slope of the curves, is very high during the first hours and slowly decreases to almost zero after a contact time of several days. Gupta and Balomajumder [27] and Ullah, et al. [28] reported the same trends in their studies. This characteristic is probably due to the large availability of sorption sites on the surface of the CSH whereas sites located inside the particle are much less accessible due to the low grain porosity.

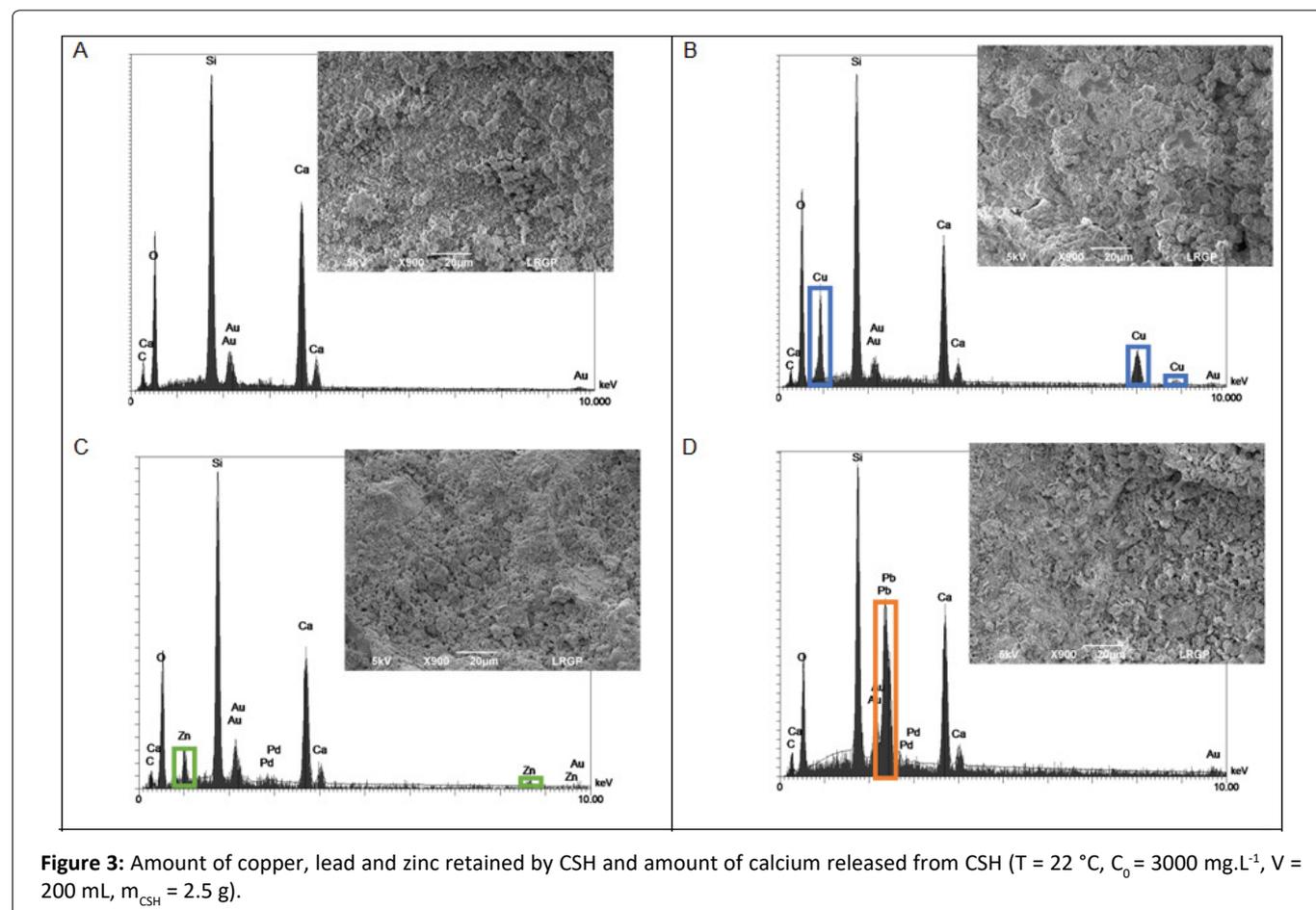
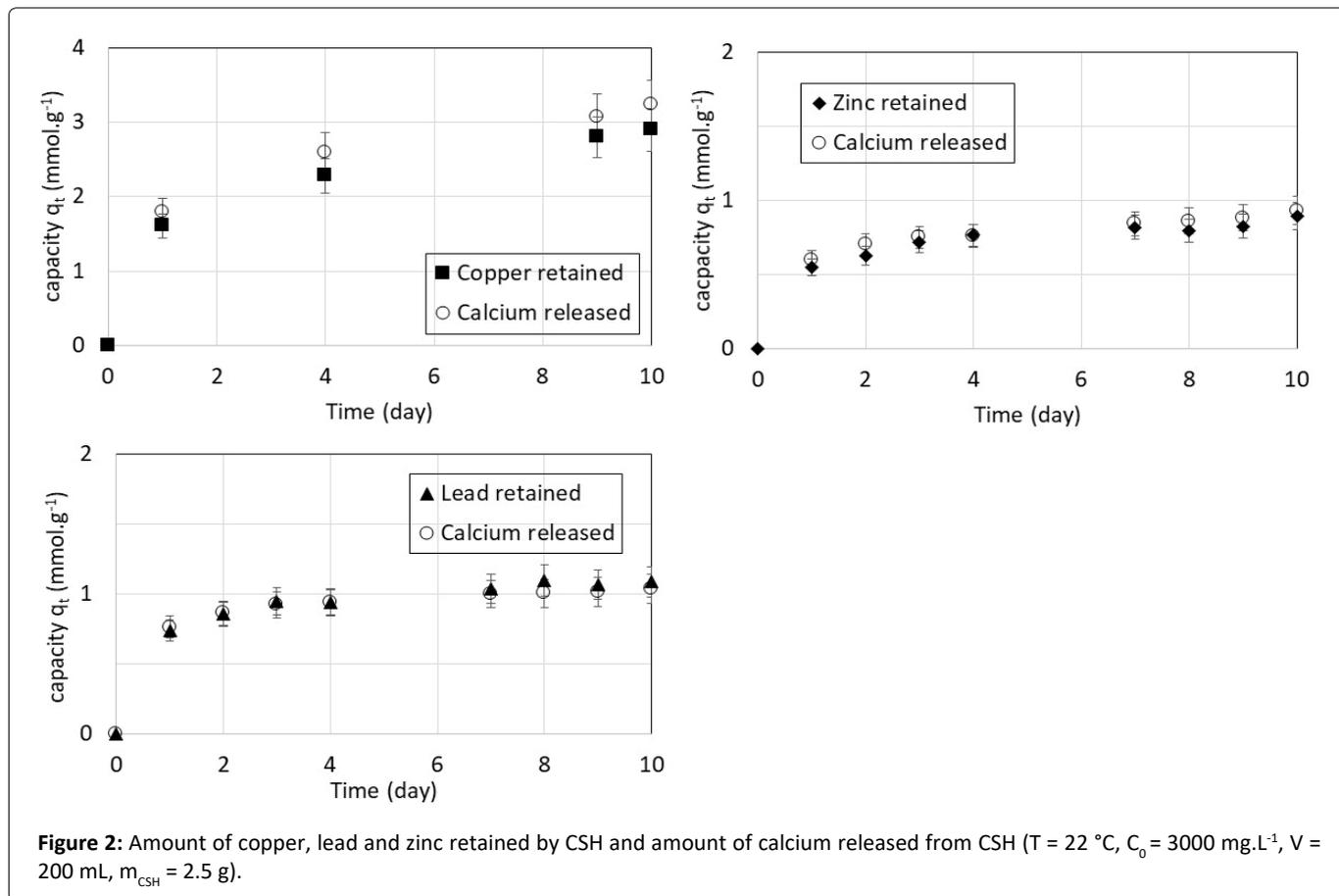
Despite the same experimental conditions used, the sorption capacities were different according to the metal retained. After ten days, 85%, 71% and 24% of Pb(II), Cu(II) and Zn(II) were respectively retained by the CSH. It can be assumed that after ten days the equilibrium was reached for all metals.

The concentration of calcium ions in solution was also measured during the experiments. Figure 2 shows the amount ( $q_t$ ) in mmol.g<sup>-1</sup> of copper, lead and zinc retained on the CSH and the corresponding amount of calcium released in the solutions during the kinetics experiments. Because the studied metals as well as calcium have a valence of 2, the amounts in mmoles are also the amounts in charge. Cu(II), Pb(II) and Zn(II) uptakes perfectly match Ca(II) release in the solutions leading to the conclusion that ion exchange is the main mechanism involved in metal uptake by CSH. This exchange can be represented by the following reaction:



with R, the CSH skeleton and M, the metal that is Cu, Pb or Zn.

This mechanism can also explain the slow kinetics ob-



served on Figure 1. The water must enter the grain to ionize calcium before ion exchange can take place. This phenomenon, well known for ion exchange resins, probably induces some modifications of the structure of CSH such as swelling and bursting of grains.

Moreover, SEM micrographs and EDX spectra of CSH material were obtained before and after sorption of Cu(II), Zn(II) and Pb(II) (Figure 3). The apparition of additional peaks on EDX spectra after metal sorption (pictures B, C and D) confirms the presence of copper, zinc and lead at the CSH surface. The intensity of Ca peak tends to decrease after metal sorption. SEM pictures also suggest a textural modification of the CSH surface after metal sorption. Some agglomerates quite homogeneously distributed appeared on the surface. Their typical shape seems to depend on the sorbate: Rather a smooth continuum for Cu or some granular growths for Pb and Zn.

In order to represent the experimental data, two well-known kinetics models (pseudo-first and pseudo-second order kinetics) based on chemical reaction process [29] and not specific to ion exchange complex process were used. For both models, the main hypotheses are that only one ion species (i.e. calcium) is exchanged with the metal, the CSH material is homogeneous and no swelling of the solid is considered.

The pseudo-first order model based on the solid capacity to sorb is expressed as:

$$\frac{dq_t}{dt} = k_1 (q_e - q_t) \quad (\text{eq.3})$$

Where  $k_1$  is the rate constant of pseudo-first order ( $\text{day}^{-1}$ ),  $q_e$  and  $q_t$  are respectively the metal amounts retained at equilibrium and at time  $t$  (day) both expressed in  $\text{mg.g}^{-1}$ . The resolution of equation 3 leads to:

$$q_t = q_e (1 - e^{-k_1 t}) \quad (\text{eq.4})$$

The pseudo-second order kinetics model based on sorption equilibrium capacity is expressed by the following equation:

$$\frac{dq_t}{dt} = k_2 (q_e - q_t)^2 \quad (\text{eq.5})$$

Where  $k_2$  is the rate constant of pseudo-second order sorption ( $\text{g.mg}^{-1}.\text{day}^{-1}$ ),  $q_e$  and  $q_t$  are the amounts of metal retained ( $\text{mg.g}^{-1}$ ) at equilibrium and at time  $t$  (day), respectively. The resolution of equation 5 results in:

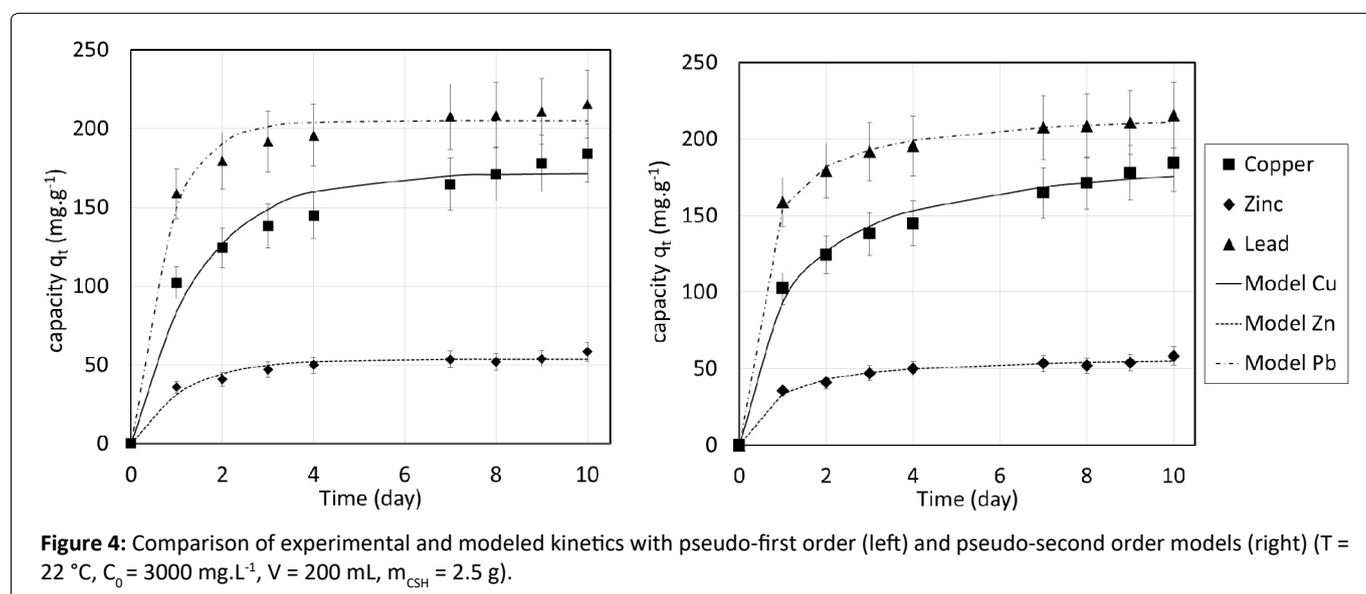
$$q_t = q_e - \frac{1}{\frac{1}{q_e} + k_2 t} \quad (\text{eq.6})$$

The model parameters were estimated by nonlinear regression using Excel solver based on the minimization of the root mean square error (RMSE) between experimental and modeled data. A combination of absolute error measurement via the RMSE and relative error measurement via the determination coefficient  $R^2$  was used to evaluate the goodness-of-fit.

The obtained parameters for both models are listed in Table 2. As shown in Figure 4, both models allowed to represent experimental data but the RMSE (Table 2) for the pseudo-first

**Table 2:** Kinetics parameters of the pseudo-first order and pseudo-second order kinetics models for the sorption of Cu(II), Zn(II) and Pb(II) on CSH ( $T = 22\text{ }^\circ\text{C}$ ,  $C_0 = 3000\text{ mg.L}^{-1}$ ,  $V = 200\text{ mL}$ ,  $m_{\text{CSH}} = 2.5\text{ g}$ ).

Pseudo-first order model	Cu (II)	Zn (II)	Pb (II)
$k_1$ ( $\text{day}^{-1}$ )	0.67	0.88	1.32
$q_e$ ( $\text{mg.g}^{-1}$ )	171	53	205
RMSE ( $\text{mg.g}^{-1}$ )	10.11	2.76	7.54
$R^2$	0.959	0.972	0.986
Pseudo-second order model	Cu(II)	Zn(II)	Pb(II)
$k_2$ ( $\text{g.mg}^{-1}.\text{day}^{-1}$ )	0.0047	0.023	0.011
$q_e$ ( $\text{mg.g}^{-1}$ )	195	59	220
RMSE ( $\text{mg.g}^{-1}$ )	5.58	1.65	2.43
$R^2$	0.987	0.991	0.998



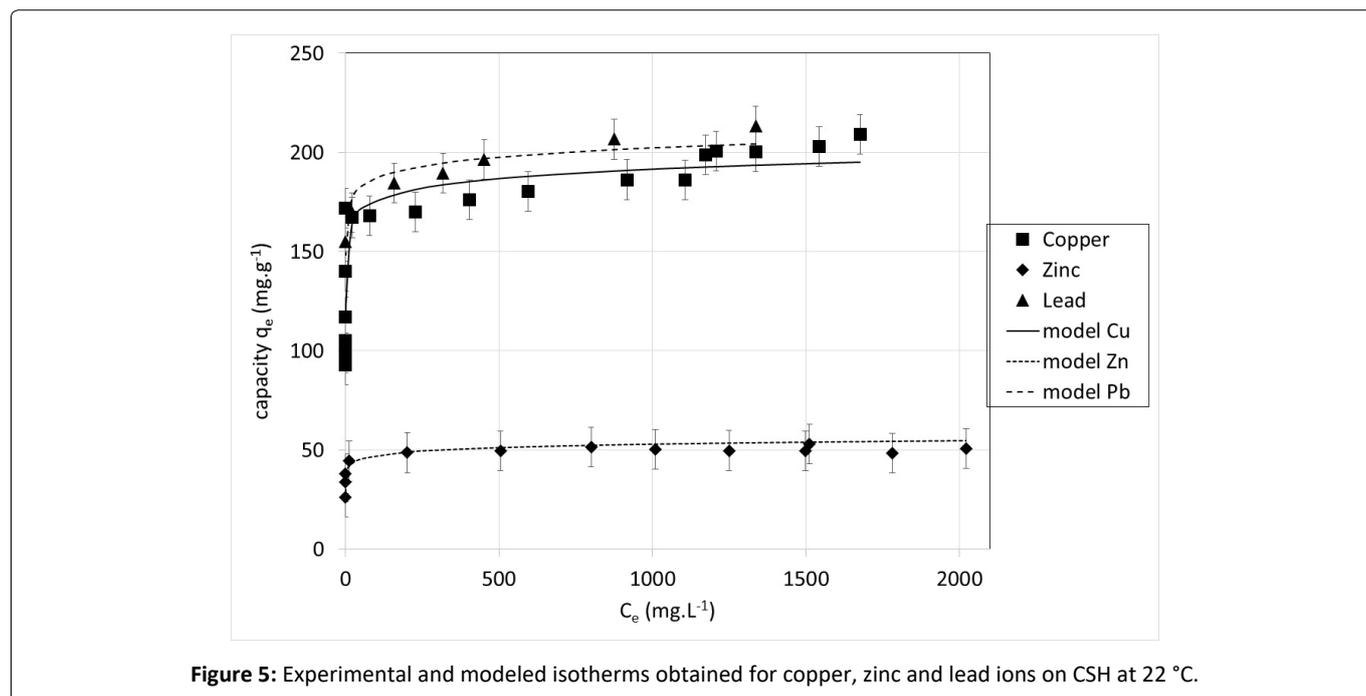


Figure 5: Experimental and modeled isotherms obtained for copper, zinc and lead ions on CSH at 22 °C.

Table 3: Maximum sorption capacities (mg.g<sup>-1</sup>) for CSH (this study) and other adsorbents.

Material	Cu capacity (mg.g <sup>-1</sup> )	Pb capacity (mg.g <sup>-1</sup> )	Zn capacity (mg.g <sup>-1</sup> )	Ref.
Zeolite (Clinoptilolite)	25.7	290.1	17.5	[23]
Zeolite (Egyptian Kaoline )	43.8	213.4	41.2	[31]
Zeolite (Chabasite)	5.1	6.0	5.5	[32]
Zeolite X	109	549		[32]
Zeolite 13X	136			[32]
Activated carbon	7.7	19.3	3.5	[24]
Clays	54.1	239	250	[33]
CSH/Chitosan	425	796	400	[24]
CSH	680		252	[26]
CSH	209 ± 21	213 ± 22	53 ± 6	This study

order are higher than the RMSE for the pseudo-second order. Moreover, the determination coefficient  $R^2$  are closer to 1 for the pseudo-second order model, meaning that it better represents experimental data. The pseudo-first order kinetics model is particularly adapted for fast sorption processes [29] which are not the case in this study where the sorption is quite slow and then better fitted by pseudo-second order kinetics model. Bonilla-Petriciolet, et al. [29] stated that the pseudo-second order kinetics model has been successfully applied to the adsorption of metal ions from aqueous solutions.

Finally, kinetics measurements showed that the mechanism involved in the metal capture is ion exchange with a release of calcium from the CSH. As for many liquid systems, the equilibrium is reached after long times even if a large decrease of the concentrations is observed after few hours for zinc, lead and copper in solution. A pseudo-second order kinetics allows the modelling of the global phenomenon probably controlled by the reaction step.

**Isotherms:** Following the described procedure, sorption isotherms representing the equilibrium capacity after 10 days ( $q_e$ ) versus the equilibrium concentration in the liquid phase ( $C_e$ ) were obtained with single metal solutions at 22 °C (Figure 5).

The obtained isotherms are all of type I according to the IUPAC classification [30]. It is important to note that the isotherms are extremely steep: Maximum sorption capacities are reached for very low concentrations. This is compatible with ion exchange mechanism while the exchanger is not close to its maximum exchange capacity (corresponding in our case to a metal deficit compared to the calcium availability). The obtained results show that the maximal weight sorption capacities were as follows: Pb(II) > Cu(II) >> Zn(II). The maximum experimental sorption capacity attained 213 mg.g<sup>-1</sup> for Pb(II), 209 mg.g<sup>-1</sup> for Cu(II) and 53 mg.g<sup>-1</sup> for Zn(II). These weight capacities were compared with previously reported data for several adsorbents (Table 3) showing that the maximum sorption capacities of the studied CSH are often greater. Unsurprisingly, activated carbons show poor performance for

metal ion removal whereas zeolites and clays have high capacities. Lead weight capacity seems to be higher than that of copper and zinc in almost all the studies.

When speaking in molar sorption capacities the order is Cu(II) >> Pb(II) > Zn(II) and the maximum experimental capacities are 3.29 mmol.g<sup>-1</sup> for Cu(II), 1.03 mmol.g<sup>-1</sup> for Pb(II) and 0.81 mmol.g<sup>-1</sup> for Zn(II). The maximum quantity of metal that is retained by the CSH can be linked to the amount of exchangeable calcium present in the solid. Thus, the amounts retained are more important in [26] for all metals as the amount of calcium is. Calculations showed that only 62%, 19% and 15% of the calcium available in the CSH is exchanged respectively for copper, lead and zinc. As in ion exchange resins [34,35], the differences between metallic ion could be correlated with the hydrated ionic radius and electronegativity of metallic species (Table 4). The retained amount tends to increase as the hydrated ionic radius decreases because smaller species make the solid structure swell less, so the work to go to equilibrium is lower. Furthermore, the greater the electronegativity of the species, the more significant the ion exchange [34,35].

Experimental isotherms are commonly represented by isotherm models, among which Langmuir model is one of the most used to model sorption equilibrium. The Langmuir theory assumes a limited and constant number of sites for exchange and that the exchange is reversible. To establish the mathematical expression of the isotherm, Langmuir admits that at all times, there is a dynamic balance between the speeds of fixation and desorption. In this case, it is a simple application of the mass action law leading to the Langmuir thermodynamic equilibrium constant defined as

$$b(L.mg^{-1}) = \frac{[fixed\ species]_{eq}}{[M^{2+}]_{eq} \cdot [vacant\ site]_{eq}}$$

As the number of sites is constant, they are either vacant or containing a fixed species. Defining  $q_e$  as the amount of retained metal at equilibrium (mg.g<sup>-1</sup>) and  $q_{max}$  (mg.g<sup>-1</sup>) as the maximum amount of retained metal, the quantity of vacant

**Table 4:** Hydrated ionic radius and electronegativity of metal species (reported from [31]).

Metal	Hydrated ionic radius (Å)	Electronegativity (kJ.mol <sup>-1</sup> )
Pb	4.01	1.8
Cu	4.19	1.9
Zn	4.30	1.6

**Table 5:** Langmuir-Freundlich parameters for the sorption of single metal ions on CSH at 22 °C.

	Cu	Zn	Pb
$q_{max}$ (mg.g <sup>-1</sup> )	356	111	489
$b$ (L.mg <sup>-1</sup> )	$7 \cdot 10^{-3}$	$3.4 \cdot 10^{-4}$	$2.2 \cdot 10^{-6}$
$n$ (-)	12.90	11.10	17.53
RMSE (mg.g <sup>-1</sup> )	16.06	4.62	6.07
R <sup>2</sup>	0.81	0.96	0.99

sites is equal to  $q_{max} - q_e$ .  $C_e$  is the metal concentration at equilibrium in solution (mg.L<sup>-1</sup>). With these definitions, the Langmuir equation is expressed as:

$$q_e = \frac{q_{max} b C_e}{1 + b C_e} \quad (eq.7)$$

Langmuir model assumes that the surface is homogeneous in terms of sorption energy, the sorption is localized and each site can accommodate only one molecule. In the case of CSH, the last two assumptions seem appropriate but the first one could be far from the experimental system. To take into account the heterogeneity of the sorption, the Langmuir-Freundlich model was developed (eq. 8).

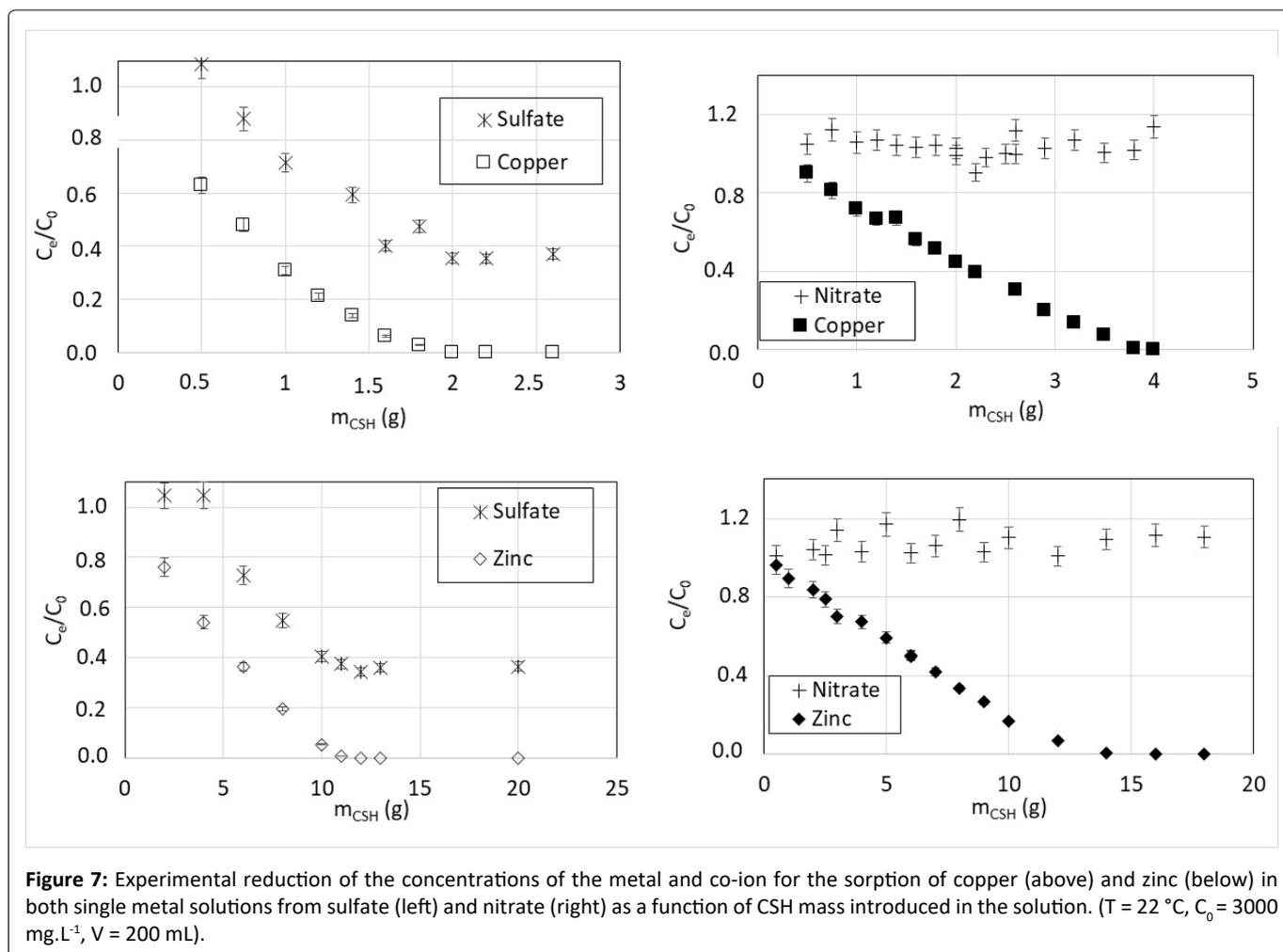
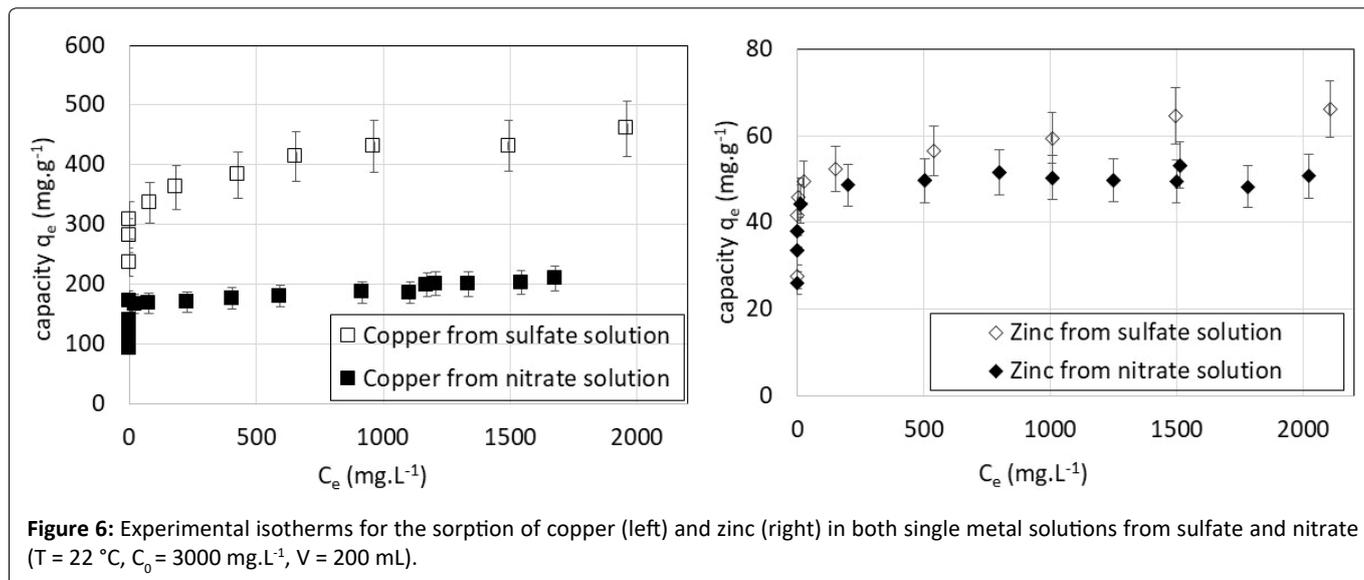
$$q_e = q_{max} \frac{(b C_e)^{1/n}}{1 + (b C_e)^{1/n}} \quad (eq.8)$$

Where  $n$  (-) represents the surface heterogeneity. Once again, Langmuir-Freundlich parameters were determined by adjusting equation 8 to experimental values minimizing the RMSE value using Excel solver. The obtained parameters for each metal are collected in Table 5. All the determination coefficient R<sup>2</sup> are superior to 0.8 signifying that the Langmuir-Freundlich model represents properly the experimental data. One can note that  $n$  parameters are really higher than 1 for the three metals, which confirms that the surface of CSH cannot be assimilated to a homogeneous one.

### Influence of the co-ion

Metal ions in solution are accompanied by an equivalent opposite charge amount of so-called co-ions. Sorption isotherms were also determined at 22 °C for Cu(II) and Zn(II) using solutions prepared from sulfate salts in place of nitrate (Figure 6). As predicted by the literature [31], ion exchange is favored by co-ions of higher valence. This is very impacting for copper whose capacity is doubled when associated with sulfate (SO<sub>4</sub><sup>2-</sup>) instead of nitrate (NO<sub>3</sub><sup>-</sup>). The effect of the co-ion is significantly weaker for Zn(II).

Another point to note is the decrease of the concentration of sulfate anions in the solution as CSH mass increases whereas the concentration of nitrate anions remains constant for both Zn(II) and Cu(II) (Figure 7). As the solution stays electro-neutral, the decrease of sulfate ion concentration is probably due to calcium sulfate precipitation. Indeed, this observation can be linked to the poor solubility of calcium sulfate compared to calcium nitrate (respectively about 2.1 g.L<sup>-1</sup> and 1212 g.L<sup>-1</sup> at 20 °C). A part of sulfate ions precipitates with calcium ion excess released by ion exchange with metal cations (Cu<sup>2+</sup> or Zn<sup>2+</sup>) leading to a joint reduction of the metal and sulfate ions. Considering that the molar amount of Ca<sup>2+</sup> released is equal to the amount of M<sup>2+</sup> captured and knowing the calcium sulfate solubility, it is possible to calculate the quantity of sulfate precipitating. Thus, the theoretical remaining soluble sulfate concentration ( $C_e$ ) corresponds to 33% of the initial sulfate concentration ( $C_0$ ) that is consistent with the value of approximately 36% reported on Figure 7 for high CSH masses whatever the metal.



### Influence of the presence of several metal ions

According to Mishra, et al. [36] and Jha, et al. [37], the presence of other cations in the solution results in the reduction of the maximum sorption capacity for each metal compared to that obtained in single metal solutions.

In order to investigate the influence of the presence of

competing heavy metal ions on the individual sorption of Cu(II), Zn(II) and Pb(II) by CSH, experiments were carried out with a solution containing a mixture of the three metals prepared from nitrate salts. The initial concentration of each metal was  $3000\text{ mg.L}^{-1}$  and the experiment was conducted for three masses of CSH, namely 2.5 g, 6 g and 12.5 g. Figure 8 shows the sorption kinetics of each heavy metal present in

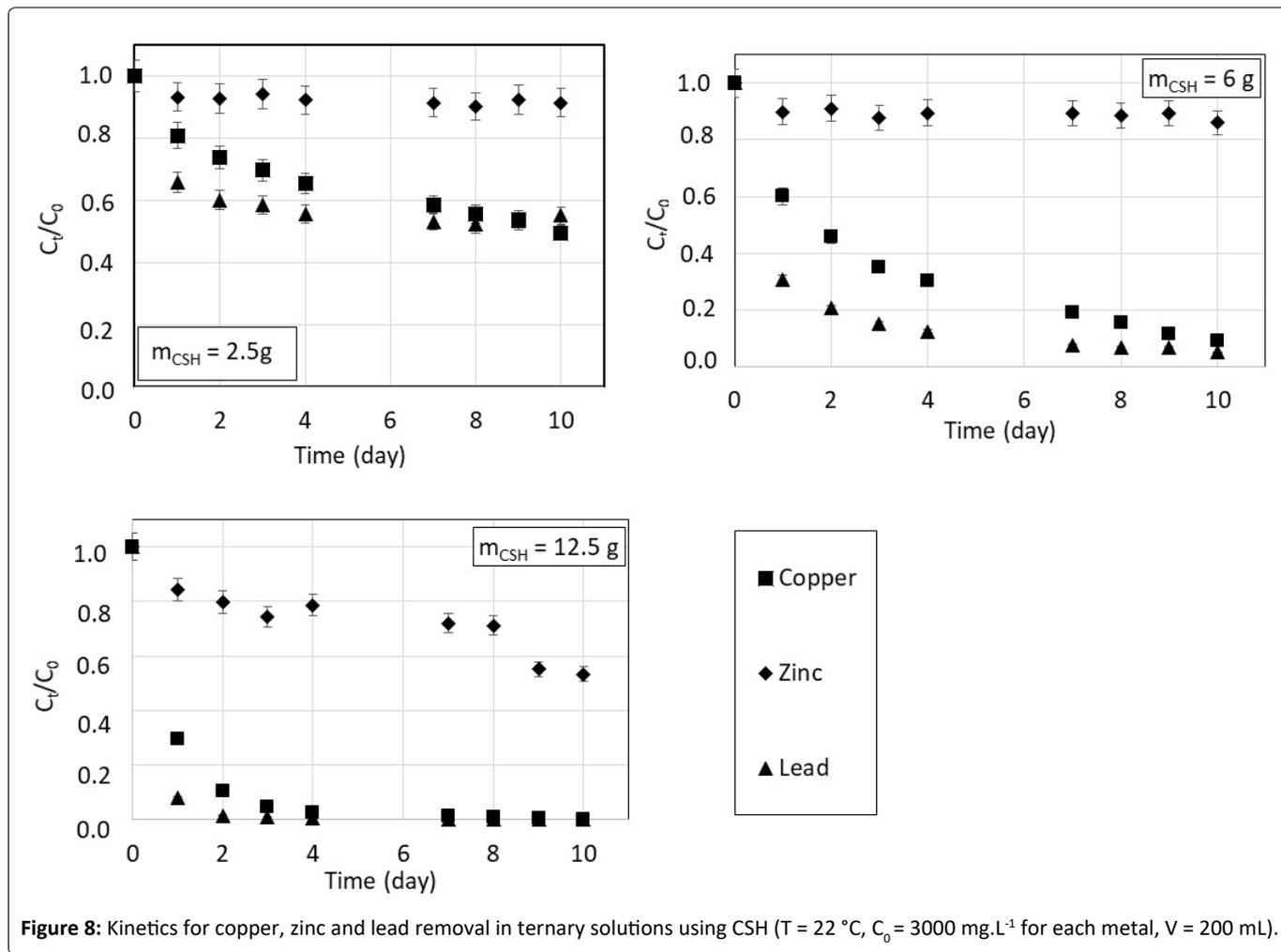


Figure 8: Kinetics for copper, zinc and lead removal in ternary solutions using CSH ( $T = 22\text{ }^\circ\text{C}$ ,  $C_0 = 3000\text{ mg}\cdot\text{L}^{-1}$  for each metal,  $V = 200\text{ mL}$ ).

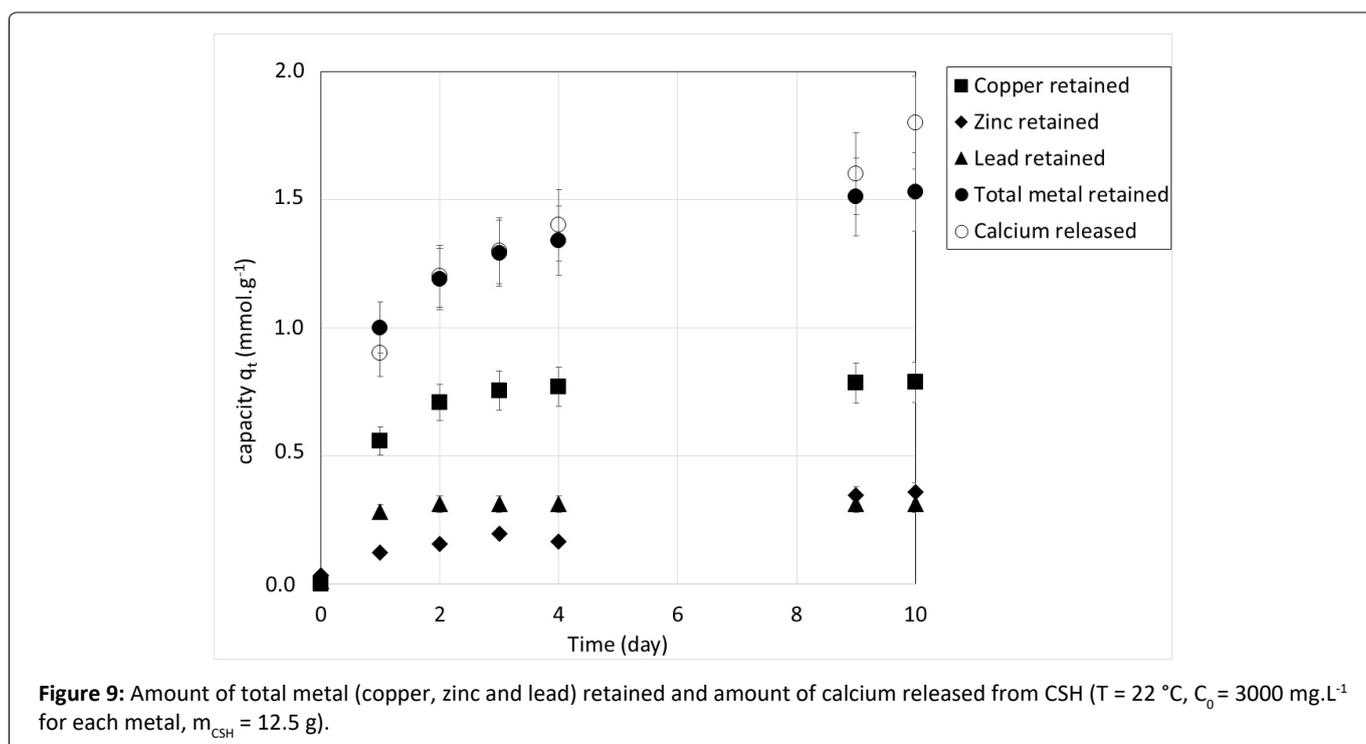


Figure 9: Amount of total metal (copper, zinc and lead) retained and amount of calcium released from CSH ( $T = 22\text{ }^\circ\text{C}$ ,  $C_0 = 3000\text{ mg}\cdot\text{L}^{-1}$  for each metal,  $m_{CSH} = 12.5\text{ g}$ ).

the mixture. For each ionic species, the greater the mass of CSH, the more rapid and better the removal from the solu-

tion. A comparison of Figure 1 and Figure 8 shows that the sorbed quantities of each ion are lower when they are in

mixture revealing a competitive effect. Moreover, the experiments showed that zinc kinetics is much lower. This is probably due to its lower mobility. To be sorbed, zinc ions must reach the least available calcium sites or wait for copper and lead concentrations to be very low. This kinetics selectivity has an important impact on zinc removal which is the most affected by the presence of other metals in solution. For all experimental conditions, one can consider that after 10 days, a pseudo equilibrium is reached.

In the case of a mixture, Figure 9 shows the amount of total metal (copper, zinc and lead) retained on the CSH and the amount of calcium released to the solution during a kinetics experiment. Once more, the correspondence of the uptake of total metal from the solution with the release of Ca(II) by CSH confirms the presence of ion exchange mechanisms in the metal sorption process.

The sorption isotherms obtained with ternary metal solutions using CSH are shown in Figure 10. This figure represents the quantity of a metal sorbed at the equilibrium versus its concentration at the equilibrium in the liquid phase in the

presence of other metal ions. The comparison of Figure 5 and Figure 10 highlights that the sorption capacity at equilibrium for each metal ion is significantly reduced in ternary solution.

Maximal sorption capacities of each metal are reported in Table 6. The proportion of metal retained in mixture compared to single metal solutions decreased as follows: Zn(II) > Pb(II) > Cu(II).

The elementary analysis of the CSH material showed that there is approximately 5 mmol of calcium per gram of solid. The experiments carried out with single metal ions make it possible to exchange  $3.3 \text{ mmol.g}^{-1}$  with copper. In a competitive ternary mixture, Table 6 shows that the total amount of calcium exchanged is similar ( $3.1 \text{ mmol.g}^{-1}$ ). Therefore, the amount of each retained metal decreases but the total capacity remains constant corresponding to approximately 60% of the calcium available in the CSH.

## Conclusion

This study showed that metal removal from aqueous solutions by CSH is performed by ion exchange with calcium from

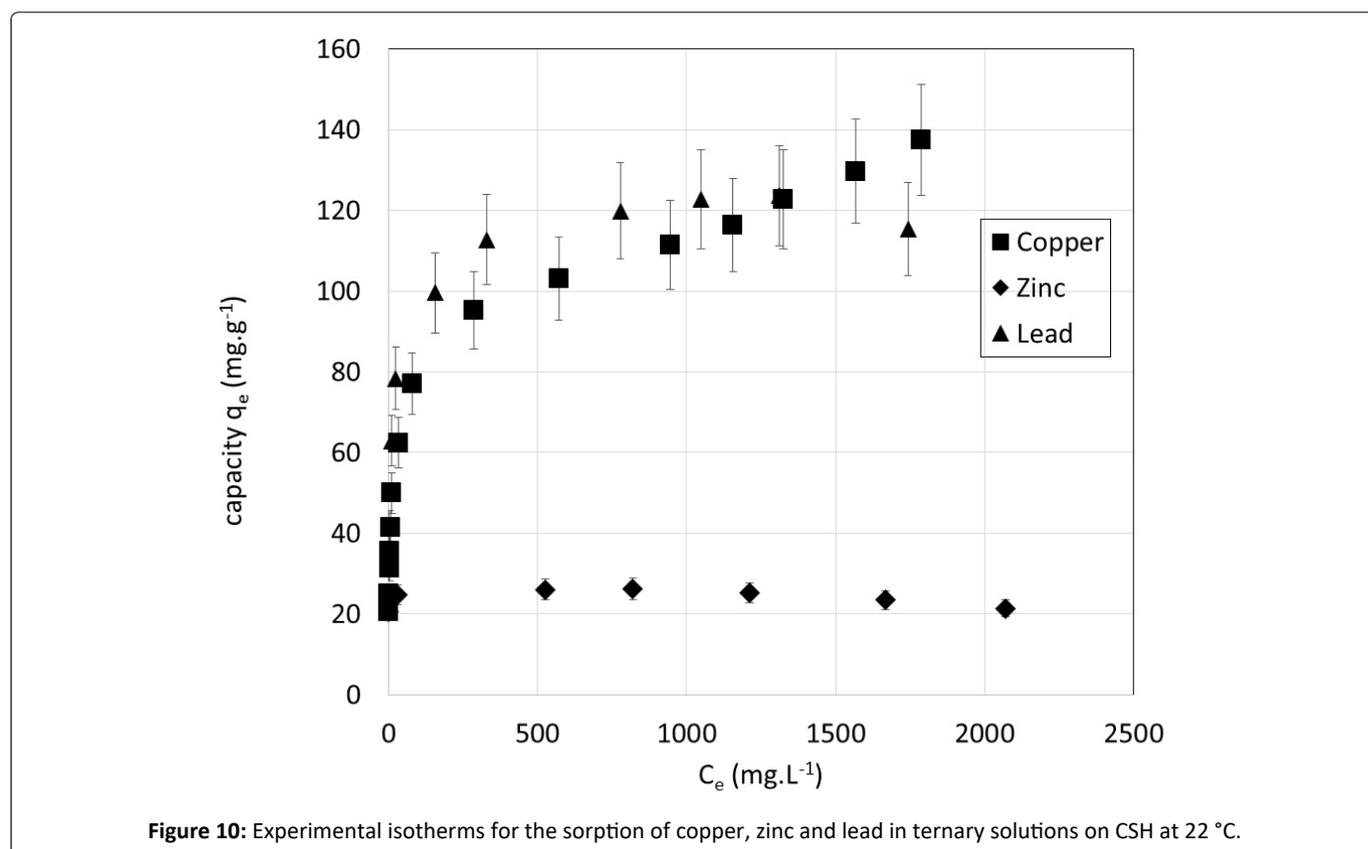


Figure 10: Experimental isotherms for the sorption of copper, zinc and lead in ternary solutions on CSH at 22 °C.

Table 6: Maximal sorption capacities (single metal and ternary solutions) at 22 °C.

Metal	Single metal solution		Ternary solution		Decrease (%)
	mg.g <sup>-1</sup>	mmol.g <sup>-1</sup>	mg.g <sup>-1</sup>	mmol.g <sup>-1</sup>	
Pb(II)	213 ± 22	1.03 ± 0.11	115 ± 12	0.55 ± 0.06	46
Cu(II)	209 ± 21	3.29 ± 0.33	137 ± 14	2.16 ± 0.22	34
Zn(II)	53 ± 6	0.81 ± 0.08	23 ± 3	0.35 ± 0.04	56
Total				3.06 ± 0.32	

the material.

Whatever the metal, the transfer kinetics, properly represented by pseudo-second order kinetics model, is quite slow, even more for zinc. Even if more than 50% (between 55% and 75%) of the removal potential is expressed during the first hours, it is necessary to wait ten days to reach the equilibrium. Therefore, for the conception and development of *in-situ* runoff water treatment solution, it is essential to allow enough contact time to take advantage of the whole CSH capacity.

The differences observed between each metal equilibrium molar capacity can be linked to their structural properties, in particular their hydrated ionic radius and electronegativity. The isotherms emphasized that the equilibrium weight capacity is higher for lead than for copper than for zinc. At saturation, about 60% maximum of the calcium available in the CSH is used for ion exchange. The maximum metal weight capacities obtained experimentally are comparable or even higher than those found in the literature for conventional materials such as zeolites and activated carbons, commonly used for water treatment. In terms of thermodynamics, this low cost adsorbent (whose basic composition could easily be found in industrial residues) has an interesting potential.

An important impact of the co-ions present in solution was underlined, particularly for copper whose maximal weight capacity was doubled in the presence of sulfate rather than nitrate ions of lower valence. Calcium sulfate precipitation phenomenon was also observed.

Competition phenomena were highlighted in the case of metal mixture. Even if the total retention capacity is not affected, the maximum single uptakes for each metal are reduced. Zinc removal is mainly impacted due to kinetics selectivity partly associated to its physicochemical properties.

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