



## Review Article

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# Mass Loss of a Polymeric Composite under Action of Space Radiations

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## Abstract

The effect of electron, proton and electromagnetic radiations on mass loss of EKOM-1 polymeric composite was studied. Irradiation was made by 40-keV electrons and protons and electromagnetic radiation in vacuum chamber of the "UV-1/2" test facility. It was found that parameters characterizing the synergistic effects of mass loss of the material for stated conditions of electron-proton and combined radiations are the functions of irradiation time. To interpret the experimental data, a physical-mathematical model of mass loss of polymeric materials in vacuum was proposed. The obtained data can be explained by diffusion fluxes associated with the gradient of concentration of radiolysis products and increase of gas permeability of a material under radiation.

## Keywords

Space radiations, Composite, Thermal control coating, Mass loss, Volatile products

## Introduction

Polymeric materials find ever-widening applications in space technique. This is tied with the simplicity of producing the polymeric-based composites with the predetermined set of properties. However, these materials in space become the sources of volatile products (VP) that increase density of spacecraft outer atmosphere that undermines the serviceability of the on-board equipment [1-5]. Therefore, studying the mass loss of spacecraft materials in service conditions is a vital task. For example, action of electron, proton and electromagnetic radiations on external coatings of high-elliptical and high-altitude satellites can result in noticeable growth of their mass loss. But, if actions of individual radiations on mass loss of materials in vacuum are already known in some aspects [6-11], the information on how they act in various combinations and as a whole is almost absent.

This work is devoted to studying action of separate (electron, proton, and electromagnetic), paired, and total set of radiations on mass loss of a pattern material in vacuum. The primary focus was on studying and interpretation of synergistic effects appearing in the course of mass loss of the pattern material EKOM-1 polymeric composite, the widely used spacecraft thermal control coating being a composition of acrylic copolymer and powdered zinc oxide (ZnO).

## Experimental Technique

To carry out the experiments, EKOM-1 thermal control coating (TCC) with a glass transition temperature of about

390 K was chosen as a model material. The EKOM-1 is a composite consisting of a polymeric matrix (acrylic copolymer) and a filler (ZnO particles). Weight ratio of the matrix and the filler is 1:5.5. No electrostatic discharges occur when irradiating the EKOM-1 because its specific resistance does not exceed  $5 \times 10^5$  Ohm/m. The 100- $\mu$ m thick coating was applied to the substrate made of AMg6 aluminum alloy with dia. 30 mm. This sample was clamped to the metal table that prevents charging.

Effect of radiation on mass loss of the model material was determined in two stages. At the first stage, the samples were irradiated in the vacuum chamber of the "UV-1/2" test facility (Figure 1). Together with the samples to be irradiated, the witness samples protected from radiation were also fastened to the table of the "UV-1/2". Before and after irradiation the both types of samples were weighed using the AUW-220D Shimadzu microbalances (accuracy is  $\pm 10^{-5}$  g).

The samples were irradiated under the following condi-

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tions:

- Pressure in the chamber  $10^{-4}$  Pa;
- Temperature of the table with samples was  $30 \pm 1$  °C;
- Electron and proton flux densities ( $\varphi_e$  and  $\varphi_p$ ) were  $5 \times 10^{14} \text{ m}^{-2}\text{s}^{-1}$ ;
- Electron and proton fluxes were altered from  $10^{18}$  to  $5 \times 10^{20} \text{ m}^{-2}$ ;
- UV irradiance was equal to 1 ESR (equivalence of solar radiation);

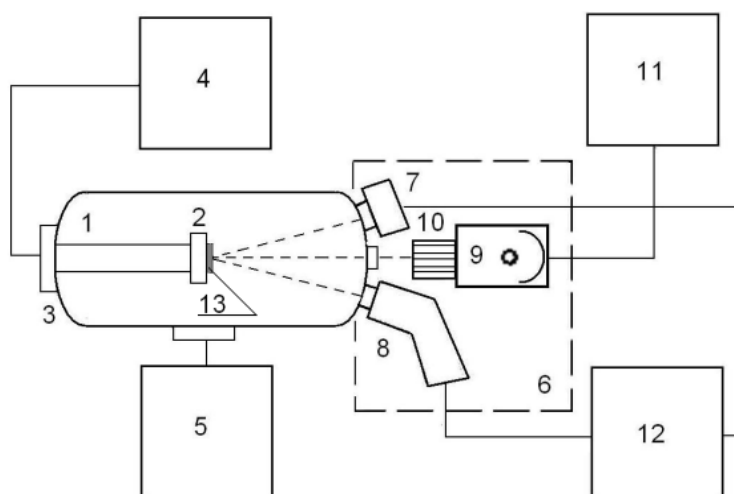
Electron ( $E_e$ ) and proton ( $E_p$ ) energies were 40 keV. These energies are characteristic for magnetospheric plasma at GSO. The purpose of the work is not an exact reproduction of radiation conditions in GEO but making a comparative anal-

ysis of mass losses of TCC being irradiated by electrons and protons of equal energies. It is obvious that major contribution to the near-surface absorbed dose of TCC make electrons and protons below 40 keV. However, the path length of protons having lesser energies is less than  $0.8 \mu\text{m}$ . This fact impedes an analysis of experimental results therefore we chose energy of 40 keV (Figure 2).

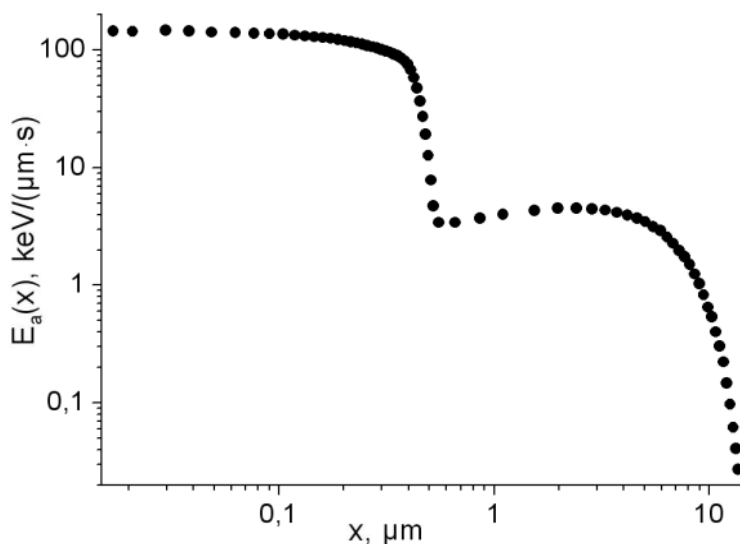
Each experiment was conducted with a batch of three or five samples. In the chapter, "Results and discussion", the average values of mass loss for three samples are presented.

## Mathematical Model

The mathematical model is based on the assumption that mass loss of a polymeric composite embraces, in general, the following processes [11]:



**Figure 1:** Schematic diagram of the "UV-1/2" test facility: 1 - vacuum chamber; 2 - table for samples; 3 - thermostat; 4 - pumping and vacuum monitoring system; 5 - measurement unit; 6 - space simulators; 7 - electron accelerator; 8 - proton accelerator; 9 - simulator of solar radiation (UV-source); 10 - forming optical device; 11 - solar simulator control box; 12 - accelerators control box; 13 - sample.



**Figure 2:** Distribution of absorbed energy in polymeric matrix of the EKOM-1 irradiated by electrons and protons ( $\varphi_e = \varphi_p = 10^4 \text{ m}^{-2}\text{s}^{-1}$ ).

- Desorption of VP adsorbed on material surface and/or formed on it under radiations;
- Diffusion and desorption of products absorbed or formed in material due to thermal decomposition and radiation;
- Sublimation of material in vacuum under radiations.

The model also postulates that  $M_i(t)$  - mass loss rate for  $i$ -type VP is proportional to its concentration in the near-surface layer of material  $C_i(l - \nu t, t)$ .

$$\dot{M}_i(t) = m_i[k_i(t) + \nu]C_i(l - \nu t, t) \quad (1)$$

Where  $m_i$  - mass of  $i$ -type molecule, g;  $\nu$  - sublimation rate of material,  $\mu\text{m/s}$ ;  $t$  - current time, s;  $l$  - material thickness,  $\mu\text{m}$ ;  $k_i(t)$  - effective desorption coefficient of  $i$ -type VP,  $\mu\text{m/s}$ .

Total mass loss from the unit surface of material  $M_{total}(t)$  by time  $t$  can be calculated as follows:

$$M_{total}(t) = \sum_{i=1}^N M_i(t) = \sum_{i=1}^N m_i \int_0^l [k_i(\tau) + \nu] C_i(l - \nu \tau, \tau) d\tau \quad (2)$$

Where  $N$  - number of types of VP in irradiated material.

Total mass of VP in a sample before radiation can be calculated

$$M_{total0} = A \sum_{i=1}^K m_i \int_0^l R_i(x) dx \quad (3)$$

Where  $A$  - surface area of sample;  $R_i$  - concentration of  $i$ -type VP in material at the initial moment;  $K$  - number of types of VP in non-irradiated material.

Thus, to find mass loss caused by  $i$ -type VP one need to know its concentration in the near-surface layer of material. Typical thickness of TCC is about 100  $\mu\text{m}$  which is many times less as compared with other linear sizes of samples. Therefore, accounting for the made assumptions the task on mass loss caused by  $i$ -type VP under radiation in vacuum is coming to solving the one-dimensional boundary value problem:

In this paper, composites with preset levels of mass loss were being modeled using the one-dimensional equations describing migration of potential out gassing products in heterogeneous materials. The coordinate-dependent diffusion

equation that was used to analyze numerically distribution of radiolysis products in a composite:

$$\frac{\partial C_i(x, t)}{\partial t} = \frac{\partial}{\partial x} \left( D_i(x, t) \frac{\partial C_i(x, t)}{\partial x} \right) - \chi_i C_i(x, t) + S_i(x) \quad (4)$$

$$x \in (0, l - \nu \cdot t), \quad t > 0, \quad \nu \cdot t < l$$

$$C_i(x, t)|_{t=0} = R_i(x) \quad x \in [0, l] \quad (5)$$

$$\left( D_i(x, t) \frac{\partial C_i(x, t)}{\partial x} + [k_i(t) + \nu] C_i(x, t) \right) \Big|_{x=l-\nu t} = 0 \quad (6)$$

$$\frac{\partial C_i(x, t)}{\partial x} \Big|_{x=0} = 0, \quad t > 0 \quad (7)$$

Where  $C_i(x, t)$  - concentration of  $i$ -type VP in material;  $\chi_i$  - chemical reaction rate with involvement of  $i$ -type VP,  $\text{s}^{-1}$ ;  $D_i(x, t)$  - effective diffusion coefficient of  $i$ -type VP,  $\mu\text{m}^2/\text{s}$ ;  $R_i(x)$  - concentration of  $i$ -type VP in material at the initial moment;  $S_i(x)$  - function of  $i$ -type VP source dependent on type of material, spectrum, content and intensity of radiation.

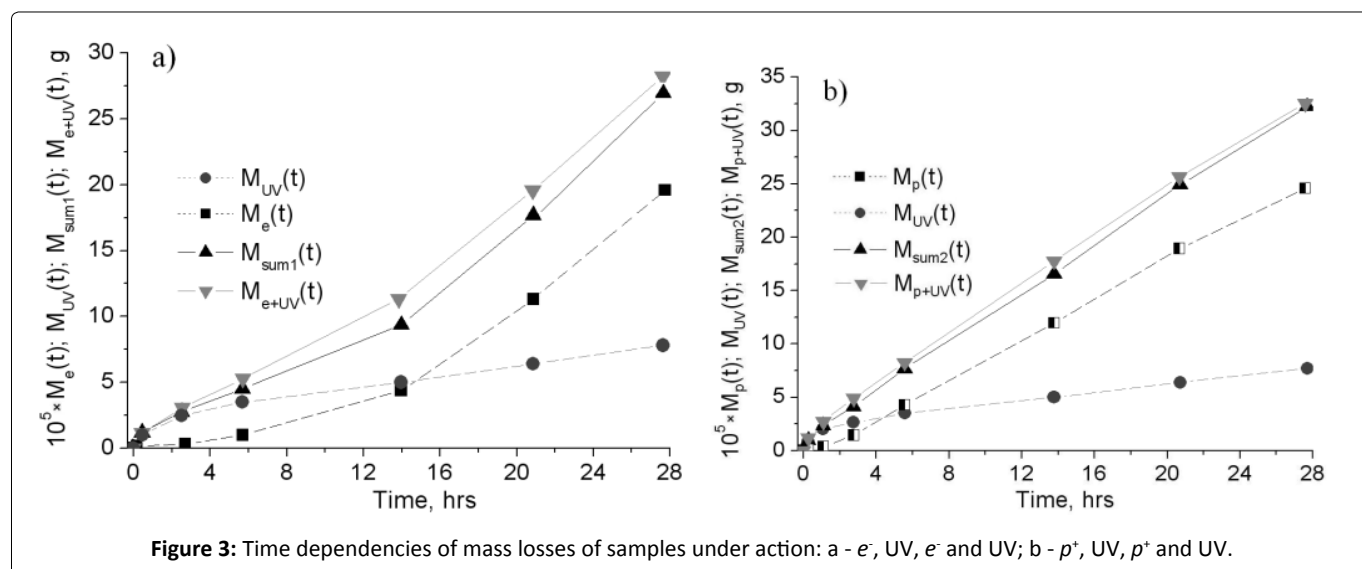
The source function  $S_i(x)$ , in its shape, repeats distribution of absorbed radiation energy in polymeric matrix of model material. Figure 3 shows distributions of absorbed energy of 40-keV electrons and protons obtained when solving the radiation transport problem by the Monte-Carlo method.

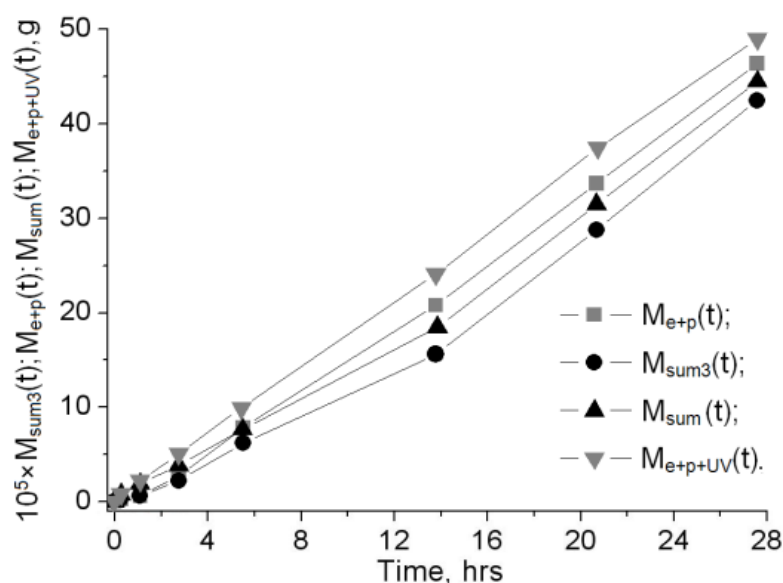
Irregularity of permeability over material thickness was taken into account by inserting the diffusion coefficient that increases with time

$$D_i(x, t) = D_{i0} [1 + \alpha_i(x) t / T] \quad (8)$$

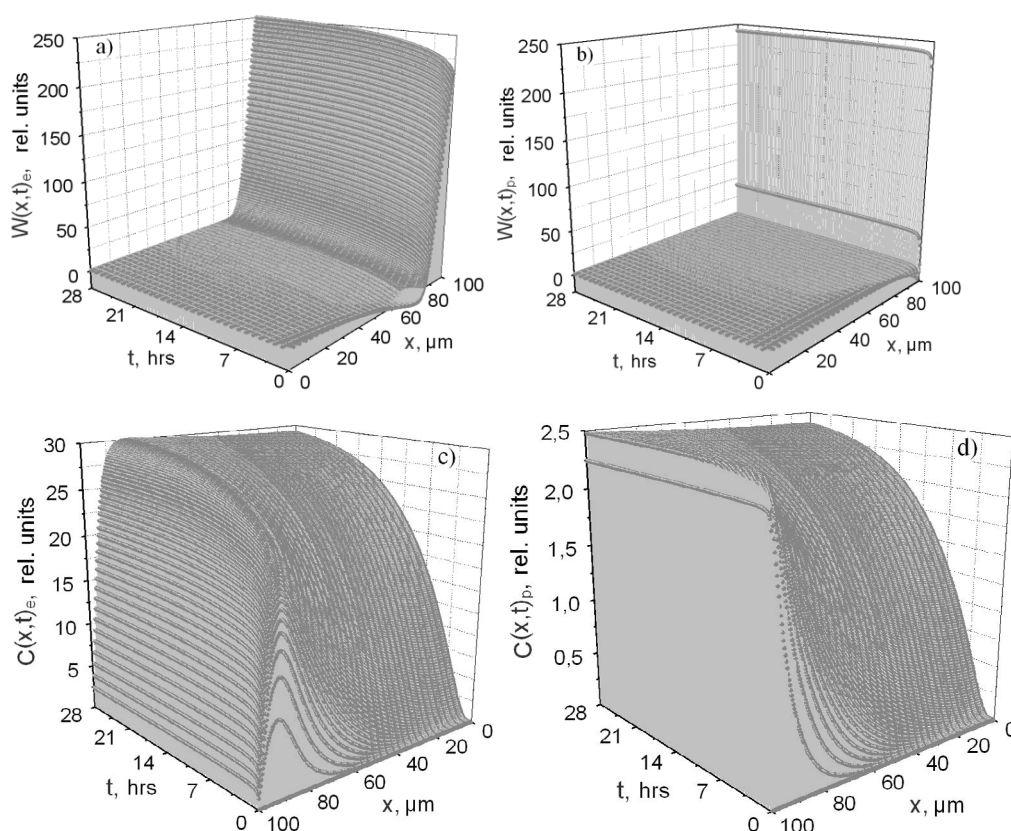
Where  $D_{i0}$  - effective diffusion coefficient of  $i$ -type VP before radiation;  $\alpha_i(x) \geq 0$  - weight function proportional to  $\varphi \cdot E_a(x)$  which represents distribution of absorbed energy rate in polymeric matrix under radiation with flux density  $\varphi$ ;  $T$  - irradiation time.

Numerical calculations quantitatively reproducing experiments were also made in two stages. The first one was dedicated to solving the set (3)-(6) that describes changes of VP concentration in material under radiation. It has been considered that VP in material before radiation was distributed uniformly.





**Figure 4:** Mass losses of samples under electron-proton irradiation.



**Figure 5:** Distribution of diffusion fluxes and CO<sub>2</sub> concentrations in samples being irradiated: a, c - by electrons; b, d - by protons.

The non-linear regression analysis methods [12,13] and the discrepancy minimization techniques were used for processing the data obtained at the second stage of experiment to precise the mathematical model parameters (1)-(8).

## Results and Discussion

In all experiments, the irradiation conditions were the

following:  $\varphi_e = \varphi_p = 5 \times 10^{14} \text{ m}^{-2}\text{s}^{-1}$  and 1 ESR. Corresponding results are given in Figure 3 and Figure 4. There were three series of experiments in which mass loss of samples under separate irradiations and their various combinations on irradiation time were studied.

- The first series: Irradiation by electrons  $M_e(t)$  (Figure 3a), protons  $M_p(t)$  (Figure 3b), UV  $M_{uv}(t)$  (Figure 3);

- The second series: Simultaneous action of electrons and UV  $M_{e+UV}(t)$  (Figure 3a), protons and UV  $M_{p+UV}(t)$  (Figure 3b), electrons and protons  $M_{e+p}(t)$  (Figure 4);
- The third series: Simultaneous action of electrons, protons and UV  $M_{e+p+UV}(t)$  (Figure 4).

The irradiation conditions were the following:  $\varphi_e = \varphi_p = 5 \times 10^{14} \text{ m}^{-2}\text{s}^{-1}$  and 1 ESR. Figure 3 shows the experimental data. The results shown here and below were found by subtracting mass loss of the reference sample  $M_0(t)$  from total mass loss of a sample at proper exposure, i.e. calculated, for example, from formulae:

$$\begin{aligned} M_e(t) &= M_{\text{total } e}(t) - M_0(t) \\ M_p(t) &= M_{\text{total } p}(t) - M_0(t) \\ M_{UV}(t) &= M_{\text{total } UV}(t) - M_0(t) \end{aligned} \quad (9)$$

Where  $M_{\text{total } e}(t)$ ,  $M_{\text{total } p}(t)$  и  $M_{\text{total } UV}(t)$  - total mass losses of samples irradiated by electrons, protons or UV respectively;  $M_0(t)$  - mass loss of the reference sample.

Thus  $M_e(t)$ ,  $M_p(t)$  and  $M_{UV}(t)$  are the mass losses of the samples due to irradiation. Having analyzed the dependencies, one can see that mass loss rate becomes almost constant very quickly under proton irradiation and increases throughout the observation period in the case of electron irradiation. It should be noted that  $M_p(t) > M_e(t)$  throughout the experiment if radiation conditions are equal. For example, mass losses of electron and proton-irradiated samples at  $t = 28 \text{ hrs}$  (it corresponds to the fluence of  $5 \times 10^{19} \text{ m}^{-2}$ ) are  $18 \times 10^{-5}$  and  $26 \times 10^{-5} \text{ g}$  respectively. Having analyzed the dependencies, one can see that mass loss rate becomes almost constant very quickly under proton irradiation and increases throughout the observation period in the case of electron irradiation. It is followed from Figure 3 that mass loss of the sample under UV at  $t = 28 \text{ hrs}$  is less than under electron (3a) and proton irradiation (3b) by 2.6 and 3.2 times respectively.

The results are explained by the fact that path lengths of 40-keV protons (0.6  $\mu\text{m}$ ) are much shorter than 40-keV electrons (16  $\mu\text{m}$ ). Therefore, the radiolysis products under the proton radiation are formed in a thinner near-surface layer of material, gas permeability of the layer growing in parallel with the absorbed dose causing the products to evolve in vacuum quicker as compared with the electron radiation. To illustrate the said, Figure 5 shows calculations of spatiotemporal distributions of diffusion flows  $W_e(x, t)$  (5a) and  $W_p(x, t)$  (5b)

$$W_e(x, t) = -D(x, t) \frac{\partial C_e(x, t)}{\partial x}, \quad (10)$$

$$W_p(x, t) = -D(x, t) \frac{\partial C_p(x, t)}{\partial x} \quad (11)$$

And concentrations (5c, 5d)  $C_e(x, t)$ ,  $C_p(x, t)$  of carbon dioxide being one of the important radiolysis products under the electron and proton radiations.

Comparing the results in Figure 5 one can see that  $W(x, t)$  in the layer that is being irradiated by electrons increases throughout the observation period and levels off quickly in the case of proton irradiation. It means that the amount of  $\text{CO}_2$  formed in material differs from the amount of  $\text{CO}_2$  evolved out in unit time

only by the amount of  $\text{CO}_2$  diffusing towards the substrate. In the case of electron irradiation, a substantial accumulation of the radiolysis products takes place (5c) in contrast with the proton irradiation. This conclusion is confirmed by experimental data (Figure 3) and calculation data of mass loss rate under irradiation.

The second series of experiments was devoted to studying the mass loss of the sample under simultaneous action of electrons and protons. Here, the fluencies and flux densities were the same as in the previous series.

Figure 4 shows dependencies of mass loss on irradiation time for electron-proton  $M_{e+p}(t)$  and combined action  $M_{e+p+UV}(t)$  as well as the values of the functions  $M_{\text{sum}3}(t) = M_e(t) + M_p(t)$ ,  $M_{\text{sum}1}(t) = M_e(t) + M_{UV}(t)$  being the sum of mass losses in the first series of experiments.

When comparing functions in Figure 4, one can see that maximum excess of  $M_{e+p}(t)$  over  $M_{\text{sum}3}(t)$  is 32% at total fluence of particles  $\Phi_{e+p} = 5 \times 10^{19} \text{ m}^{-2}$  and decreases down to 17% and 6% with the rise of  $\Phi_{e+p}$  to  $7.5 \times 10^{19} \text{ m}^{-2}$  and  $10^{20} \text{ m}^{-2}$  respectively. These data can be interpreted in assumption that combined irradiation increases permeability of material more than separate irradiations alone. Maximum effect of this on transfer of radiolysis products in material is revealed at  $\Phi_{e+p} = 5 \times 10^{19} \text{ m}^{-2}$ .

To visualize the said above, Figure 6 shows the calculation data. Here one can see that diffusion flow for the combined irradiation  $W_{e+p}(x, t)$  (Figure 6b) quickly overcomes the summarized flow  $W_{\text{sum}1}(x, t) = W_e(x, t) + W_p(x, t)$  (Figure 6a) and  $\text{CO}_2$  concentration in the material by the end of electron-proton irradiation  $C_{e+p}(x, t)$  (Figure 6d) is less than  $C_{\text{sum}1}(x, t) = C_e(x, t) + C_p(x, t)$  (Figure 6c).

Diffusive constraining of radiolysis products at initial moment of irradiation leads to their accumulation in material. However, further irradiation causes the permeability of material to increase to such extent when not only major part of volatile products evolves from it but also the products accumulated earlier. Starting from a certain moment, there sets a balance when quantity of radiolysis products forming in a sample becomes almost equal to the quantity of the products leaving it except for the ones entering the chemical reactions, i.e. mass loss rate does not change.

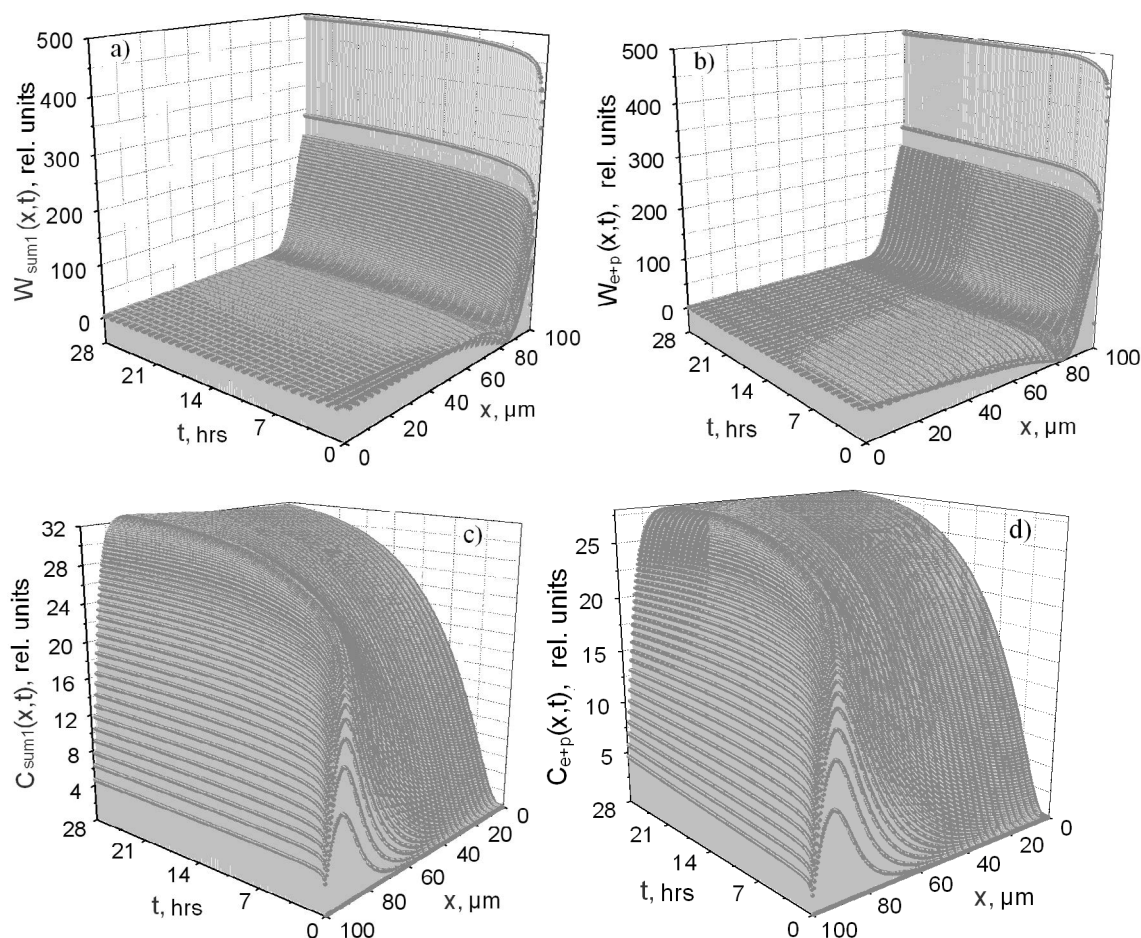
To make a quantitative estimation of synergistic effects when analyzing experimental data, we introduce the following time-dependent non-dimensional parameters.

$$\begin{aligned} a_1(t) &= \frac{M_{e+UV}(t)}{M_{\text{sum}1}(t)}; \quad a_2(t) = \frac{M_{p+UV}(t)}{M_{\text{sum}2}(t)}; \quad a_3(t) = \frac{M_{e+p}(t)}{M_{\text{sum}3}(t)}; \\ a_4(t) &= \frac{M_{\text{comb}}(t)}{M_{\text{sum}}(t)} \end{aligned}$$

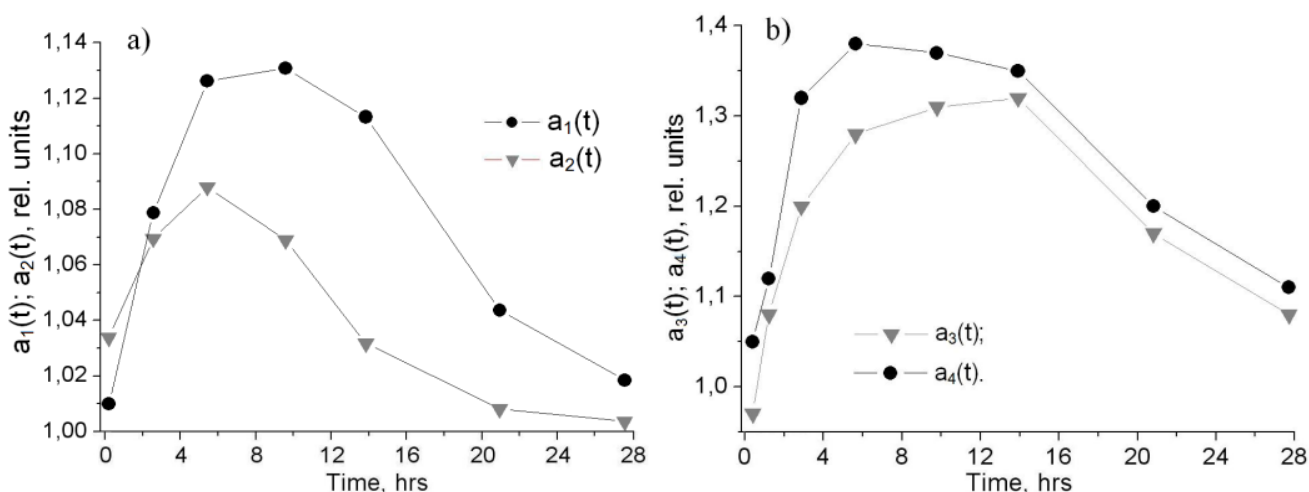
Their behavior is shown in Figure 7.

It is seen from Figure 7a that  $a_1(t) < a_2(t)$  at initial irradiation period. It is related to the fact that the radiolysis products are mostly formed far away from the surface as compared with the proton irradiation. Hence, in this case there is a time delay in their accumulation and making a contribution in mass loss.





**Figure 6:** Distribution of diffusion flows and CO<sub>2</sub> concentrations in samples under electron-proton irradiation calculated for the cases: a, c -  $D = \text{const}$ ; b, d -  $D = D(x, t)$ .



**Figure 7:** Time-dependent parameters characterizing the synergistic effects of combined irradiation: a -  $a_1(t)$  and  $a_2(t)$ ; b -  $a_3(t)$  and  $a_4(t)$ .

One can see from Figure 7b that significant differences in functions  $a_4(t)$  and  $a_3(t)$  are observed only when  $t \leq 14$  hrs; later their behaviors coincide and  $a_4(t) - a_3(t)$  does not exceed 0.03. The fact that  $a_3(t) = 0.93$  at  $t = 1$  hr is explained by the fact that radiolysis products forming under electron action in  $x < 99.4 \mu\text{m}$  do not contribute in total mass loss because the

resultant flow in this area is directed towards the substrate (see Figure 6b). Value of  $a_3(t)$  exceeds 1 with the rise of fluence, growth of accumulated products and permeability of the material.

The contribution of UV in mass loss of material is quite likely to be tied with additional warming-up and activation of

migration processes within the layer under irradiation. This, in turn, stimulates the migration processes in this layer and the desorption from the surface, which, in particular, is manifested itself in that  $a_4(t) - a_3(t) = 0.18$  at  $t = 1$  hr.

## Conclusion

The presence of synergistic effects in mass loss processes by EKOM-1 thermal control coating exposed in vacuum to electron-proton and combined irradiation was shown in the study. It was stated that under fixed irradiation conditions the parameters characterizing amount of effects are the functions dependent mainly on the electron and proton fluencies. It was found for the studied material that maximal synergistic effects under electron-UV, proton-UV, electron-proton and combined actions took place in different irradiation periods when the parameters are  $a_1(t = 14 \text{ hrs}) = 1.13$ ,  $a_2(t = 6 \text{ hrs}) = 1.09$ ,  $a_3(t = 14 \text{ hrs}) = 1.32$ ,  $a_4(t = 6 \text{ hrs}) = 1.38$  respectively.

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